
(12) UK Patent Application (19) GB (11) 2 048 154 A

(21) Application No 8010614
(22) Date of filing 28 Mar 1980
(30) Priority data
(31) 34101
(32) 30 Apr 1979
(31) 35025U
(32) 30 Apr 1979
(33) United States of America
(US)

(43) Application published
10 Dec 1980

(51) INT CL³
B29G 3/00

(52) Domestic classification
B5A 1R214B 1R214F
1R314C5 1R322 1R422
T14P

(56) Documents cited
None

(58) Field of search
B5A

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**(54) Reaction Injection Molded
Polyurethane Elastomers**

(57) A method of making reaction
injection molded polyurethane articles
comprises injecting into a mould a
high molecular weight polyol, a low

molecular weight active hydrogen
containing compound having a
functionality of at least two, and an
aromatic polyisocyanate, the moulded
product being post cured by
subjecting it to an ambient
temperature of from 290—425°F
(143 to 219°C).

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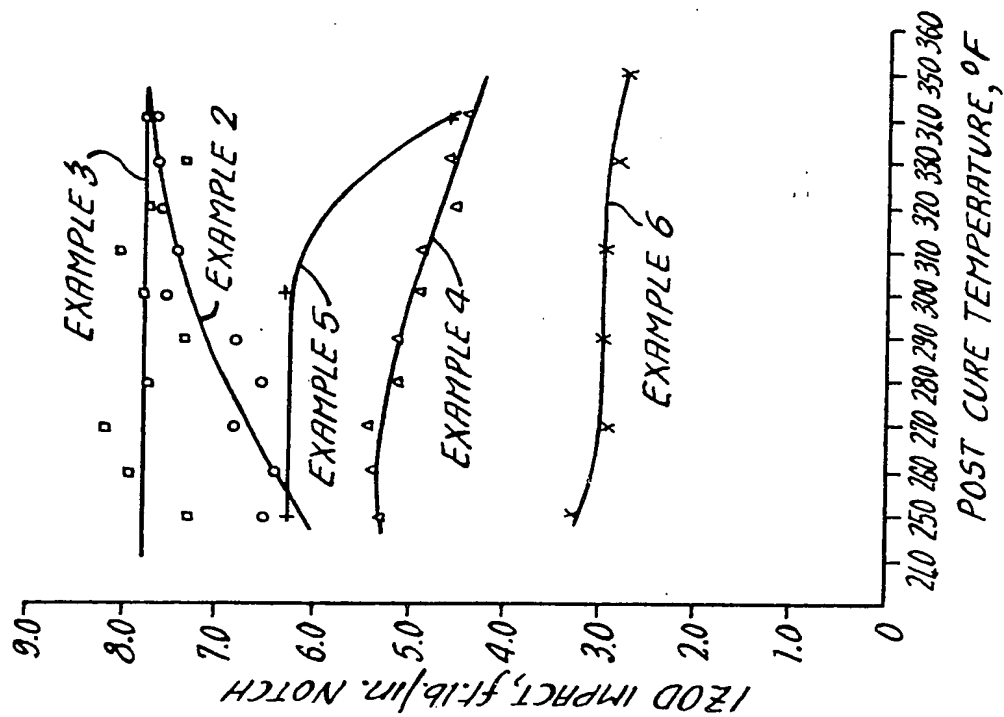


FIG.2

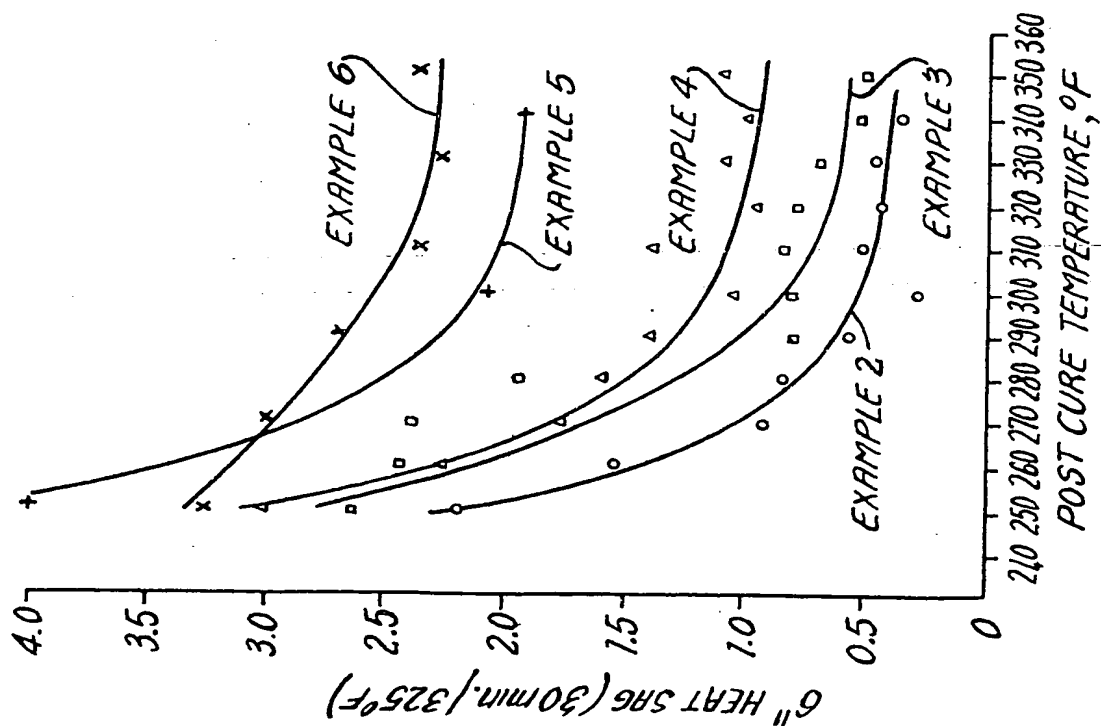


FIG.1

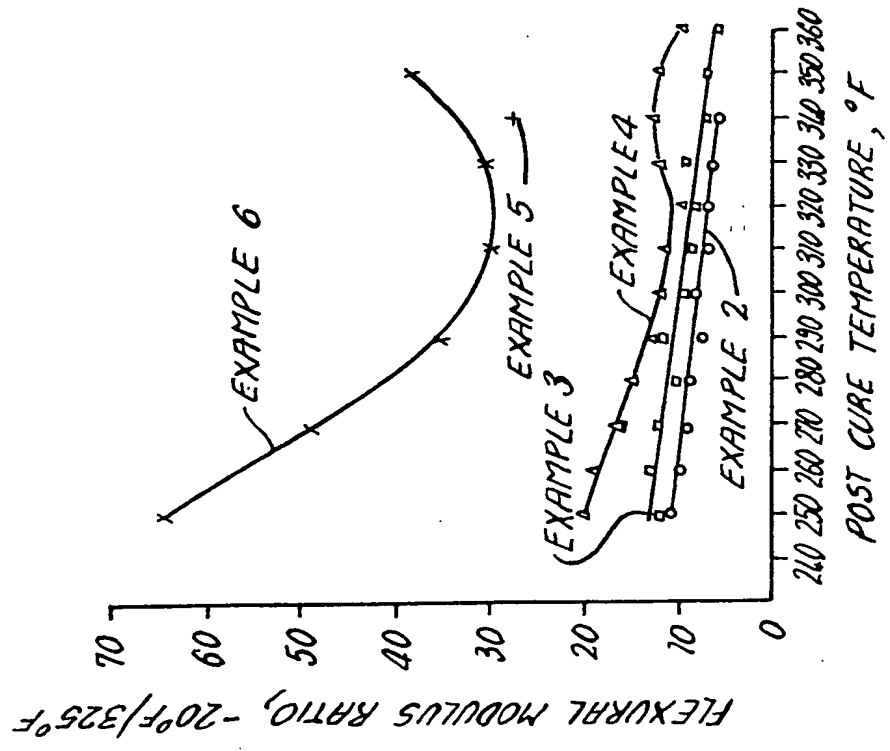


FIG. 4

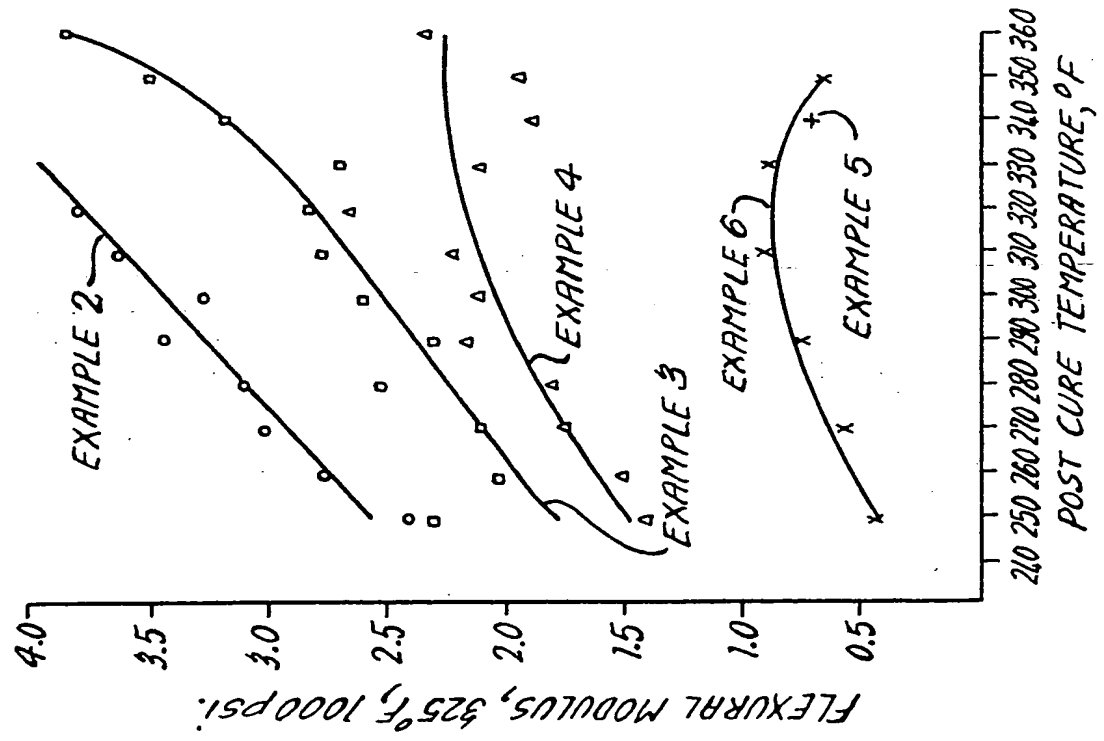


FIG. 3

SPECIFICATION

Heat Stable Reaction Injection Molded Elastomers

The invention concerns the field of reaction injection molded polyurethanes.

Reaction Injection Molding (RIM) is a technique for the rapid mixing and molding of large, fast curing urethane parts. RIM polyurethane parts are used in a variety of exterior body applications on automobiles where their light weight contributes to energy conservation. RIM parts are generally made by rapidly mixing active hydrogen-containing materials with polyisocyanate and placing the mixture into a mold where reaction proceeds. After reaction and demolding, the parts may be subjected to an additional curing step which has generally comprised placing the parts in an ambient temperature of about 250°F. (121°C). Indeed, the standard industry practice has been to post cure RIM parts at 250°F (121°C). The article "Processing and Properties of a Microcellular Foam System with Low Sensitivity to Temperature", Robert L. McBrayer and Gary J. Griffin, Journal of Cellular Plastics, July through August 1977, reveals temperatures up to 300°F (149°C). However, the article indicates that temperatures greater than 250°F (121°C) may not be practical due to part distortion. U.S. Patent No. 4,098,773 refers to heating RIM elastomers in the reaction mold without waiting for the reaction to complete at temperatures ranging from 212 to 392°F (100 to 200°C). The patent states that preferably this curing/reacting temperature is from 212 to 300°F (100 to 149°C). However, in the only examples where parts were actually heated in this manner, temperatures of only 212° and 248°F (100 and 120°C) were used.

It has been surprisingly discovered that RIM polyurethane parts may be post cured at temperatures well above 300°F (149°C) and that a substantial improvement in properties takes place due to the high post curing temperature.

The invention relates to a method of making a polyurethane elastomer of improved properties which comprises injecting an aromatic polyisocyanate, a polyol of about 500 equivalent weight and a chain-extending agent comprising a low molecular weight active hydrogen containing component having a functionality of at least two, into a mold cavity of a desired configuration demolding the resulting molded article and post curing the demolded article at a temperature from 290 to 425°F (143 to 219°C). Preferably the post curing temperature is 310 to 350°F, (154 to 177°C). The invention also provides the resulting RIM polyurethane parts.

The invention is further illustrated by the accompanying drawings in which Figure 1 shows the effect of post cure temperature on Heat Sag for various RIM parts. Figure 2 shows the effect of post cure temperature on Izod Impact. Figure 3 shows the effect of post cure temperature on Flexural Modulus. Figure 4 shows the effect of post cure temperature on the Flexural Modulus ratio at -20°F (-29°C) and 325°F (163°C).

An object of this invention is to produce RIM polyurethane parts which have improved high temperature performance. For example, an automobile exterior body panel may be prepared by this invention which could be assembled on an automobile, painted, and baked at 325°F (163°C) to cure the paint. Prior art RIM polyurethane parts would distort at this high paint curing temperature, which is normally reserved for metal parts. However, the RIM parts prepared according to this invention remain stable even at this high temperature. Even more surprisingly, formulations prepared according to this invention exhibit excellent dimensional stability and stiffness at temperatures of 325°F (163°C) or higher with no significant sacrifice in overall properties and even display improved Izod impact properties. Prior art RIM polyurethane materials have been unable to withstand the severe paint baking conditions that our materials endure without adverse effect. Also, in softer RIM formulations for automobile fascias, significant improvement in 250°F (121°C) heat stability are observed when RIM parts are prepared according to this invention. Therefore, it is an object of this invention to prepare RIM polyurethane elastomers having significantly improved high temperature dimensional stability and stiffness.

It was surprisingly discovered that a significant improvement in high temperature performance of RIM polyurethane elastomers was gained by curing the demolded elastomers at 290°F to 425°F (143 to 219°C) and preferably, from about 310°F to 350°F (154 to 177°C) rather than the industry standard of 250°F (121°C). As will be shown in the examples which follow, the improved properties are noted with a wide variety of formulations. However, some formulations are particularly preferred because their property improvements are outstanding even when compared to improved parts made according to this invention. The preferred reactants for this invention are those which yield an isocyanate-chain extender reaction with a high glass transition temperature. This glass transition temperature should be above the maximum ambient temperature to which the finished product will be subjected. For example, a paint oven is normally operated at about 325°F (163°C). The preferred polyols are those which do not significantly adversely affect the glass transition temperature of the isocyanate-chain extender reaction.

The polyols useful in the process of this invention include polyether polyols, polyester diols, triols, tetrols, etc., having an equivalent weight of at least 500, and preferably 1000 to 3000. Those polyether polyols based on trihydric initiators, having a molecular weight of 4000 and above are especially preferred. The polyethers may be prepared from ethylene oxide, propylene oxide, butylene

oxide or mixtures of propylene oxide, butylene oxide and/or ethylene oxide. In order to achieve the rapid reaction rates which are normally required for molding RIM polyurethane elastomers, it is preferable that the polyol be capped with enough ethylene oxide to increase the reaction rate of the polyurethane mixture. Normally at least 50% primary hydroxyl is preferred, although amounts of primary hydroxyl less than this are acceptable if the reaction rate is rapid enough to be useful in industrial applications. Other high molecular weight polyols which may be useful in this invention are polyesters or hydroxyl-terminated rubbers (such as hydroxyl-terminated polybutadiene). Hydroxyl terminated quasi-prepolymers of polyols and isocyanates are also useful in this invention.

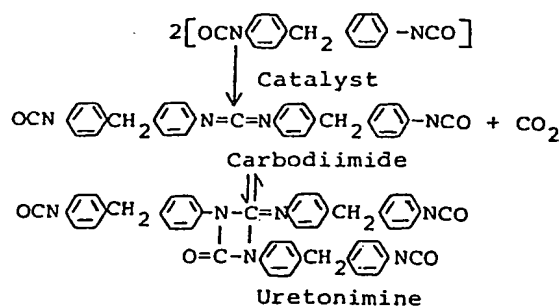
The chain-extenders useful in the process of this invention are preferably difunctional. Mixtures of difunctional and trifunctional chain-extenders are also useful in this invention. The chain-extenders useful in this invention include diols, amino alcohols, diamines or mixtures thereof. Low molecular weight linear diols such as 1,4-butanediol and ethylene glycol have been found suitable for use in this invention. Ethylene glycol is especially preferred. These chain-extenders produce a polymer having a high glass transition temperature and/or high melting point when reacted with a suitable diisocyanate to be discussed below. It has been discovered that the polyurethane polymers of this invention which have a high glass transition temperature and a high melting point also show the improved properties in the process of this invention. Other chain-extenders including cyclic diols such as 1,4-cyclohexane diol and ring containing diols such as bishydroxyethylhydroquinone, amide- or ester-containing diols or amino alcohols, aromatic diamines and aliphatic amines would also be suitable as chain-extenders in the practice of this invention.

A wide variety of aromatic polyisocyanates may be used here. Typical aromatic polyisocyanates include p-phenylene diisocyanate, polymethylene polyphenylisocyanate, 2,6-toluene diisocyanate, dianisidine diisocyanate, bitolylene diisocyanate, naphthalene-1,4-diisocyanate, bis(4-isocyanatophenyl)methane, bis(3-methyl-3-isocyanatophenyl)methane, bis(3-methyl-4-isocyanatophenyl)methane, and 4,4'-diphenylpropane diisocyanate.

Other aromatic polyisocyanates used in the practice of the invention are methylene-bridged polyphenyl polyisocyanate mixtures which have a functionality of from 2 to 4. These latter isocyanate compounds are generally produced by the phosgenation of corresponding methylene-bridged polyphenyl polyamines, which are conventionally produced by the reaction of formaldehyde and primary aromatic amines, such as aniline, in the presence of hydrochloric acid and/or other acidic catalysts. Known processes for preparing polyamines and corresponding methylene-bridged polyphenyl polyisocyanates therefrom are described in the literature and in many patents, for example, U.S. Patents No. 2,683,730; 2,950,263; 3,012,008; 3,344,162 and 3,362,979.

Usually methylene-bridged polyphenyl polyisocyanate mixtures contain 20 to 100 weight percent of methylene diphenyldiisocyanate isomers, with the remainder being polymethylene polyphenyl diisocyanates having higher functionalities and higher molecular weights. Typical of these are polyphenyl polyisocyanate mixtures containing 20 to 100 weight percent of methylene diphenyldiisocyanate isomers, of which 20 to 95 weight percent thereof is the 4,4'-isomer, with the remainder being polymethylene polyphenyl polyisocyanates of higher molecular weight and functionality that have an average functionality of from 2.1 to 3.5. These isocyanate mixtures are known, commercially available materials and can be prepared by the process described in U.S. Patent No. 3,362,979.

By far the most preferred aromatic polyisocyanate is methylene bis(4-phenylisocyanate) or MDI, e.g. as pure MDI, quasi-prepolymers of MDI, modified pure MDI, etc. Materials of this type may be used to prepare suitable RIM elastomers. Since pure MDI is a solid and, thus, often inconvenient to use, liquid products based on MDI are often used and are included in the scope of the terms MDI or methylene bis(4-phenylisocyanate) used herein. U.S. Patent No. 3,394,164 illustrates an example of a liquid MDI product. More generally uretonimine-modified pure MDI is included also. This product is made by heating pure distilled MDI in the presence of a catalyst. The liquid product is a mixture of pure MDI and modified MDI:

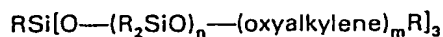


Examples of commercial materials of this type are Upjohn's Isonate 125M (pure MDI) and Isonate 143L ("liquid" MDI).

The foam formulation includes a great number of other recognized ingredients usually present in the polyol blend, such as additional cross-linkers — catalysts, extenders, and blowing agents. Blowing agents may include halogenated low-boiling hydrocarbons, such as trichloromonofluoromethane and methylene chloride; carbon dioxide, nitrogen, etc., can also be used. Catalysts such as tertiary amines or an organic tin compound or other polyurethane catalysts may be used. The organic tin compound may suitably be a stannous or stannic compound such as a stannous salt of a carboxylic acid, a trialkyltin oxide, a dialkyltin dihalide, or a dialkyltin oxide, wherein the organic groups of the organic portion of the tin compound are hydrocarbon groups containing from 1 to 8 carbon atoms. For example, dibutyltin dilaurate, dibutyltin diacetate, diethyltin diacetate, dihexyltin diacetate, di-2-ethylhexyltin oxide, dioctyltin dioxide, stannous octoate, stannous oleate, or a mixture thereof, may be used.

Tertiary amine catalysts include trialkylamines (e.g. trimethylamine, triethylamine), heterocyclic amines, such as N-alkylmorpholines (e.g., N-methylmorpholine, N-ethylmorpholine, or dimethyldiaminodiethylether), 1,4-dimethylpiperazine, triethylenediamine, and aliphatic polyamines, such as N,N,N',N'-tetramethyl-1, 3-butanediamine.

Other conventional formulation ingredients may also be employed, such as, for example, foam stabilizers, also known as silicone oils or emulsifiers. The foam stabilizer may be an organic silane or siloxane. For example, compounds may be used having the formula:



where R is an alkyl group containing from 1 to 4 carbon atoms; n is from 4 to 8; m is from 20 to 40; and the oxyalkylene groups are derived from propylene oxide or ethylene oxide. See, for example, U.S. Patent No. 3,194,773.

Although not essential for the practice of this invention, the use of commonly known additives which enhance the color or properties of the polyurethane elastomer may be used as desired. For example, chopped or milled glass fibers, chopped or milled carbon fibers and/or other mineral fibers are useful.

The RIM polyurethane elastomers of this invention are made in the conventional manner in mold and are then post cured at temperatures of about 290°F to 425°F (143 to 219°C) and preferably about 310°F to 350°F (154 to 177°C). Unexpectedly, these high post curing temperatures increase the high temperature stability of the finished RIM polyurethane elastomer. As the following examples will show, the heat sag at 325°F (163°C) is improved substantially at post curing temperatures above 290°F (143°C). Also, surprisingly, many formulations possessing this higher temperature stability show no less, and sometimes greater, Izod impact resistance when cured at the high temperatures of this invention.

Another type of additive which may be required as post curing temperatures approach 400°F (204°C) or more is an anti-oxidant. The materials which are well known to those skilled in the art include hindered phenols as well as other materials.

In a particularly preferred embodiment of this invention, a high molecular weight polyether polyurethane polyol of 5000 molecular weight or above is combined with ethylene glycol, and a standard catalyst system is combined with 4,4'-diphenylmethane diisocyanate (MDI), along with other necessary ingredients known in the art and subjected to a normal RIM molding procedure. The reacted RIM part has been removed from the mold and post cured at a temperature above 310°F (154°C) for about 30 minutes. As will be shown below such a procedure caused a striking improvement in heat sag over procedures of the prior art where lower post cured temperature is used. Also, this particular formulation showed an improvement over other formulations although all formulations tested displayed an improvement as post-curing temperature was increased.

The following examples demonstrate our invention. They are not to be construed as limiting our invention in any way but merely to be exemplary of the improvement and manner in which our invention may be practiced.

A glossary of terms and materials used in the following examples precedes the examples.

Glossary of Terms and Materials

- RIM — Reaction Injection Molding.
- Polyol — A di or greater functionality high molecular weight alcohol or amine terminated molecule composed of ether groups such as ethylene, propylene, butylene, etc., oxides.
- MDI — 4,4'-diphenyl methane diisocyanate.
- Isonate 143L — Pure MDI isocyanate modified so that it is a liquid at temperatures where MDI crystallizes — product of the Upjohn Co.
- PAPI 901 — A crude form of MDI containing about 30% higher functionality isocyanates and other impurities — product of the Upjohn Co.
- Isonate 191 — Thought to be a 50/50 blend of Isonate 143L and PAPI 901 — product of the Upjohn Co.

- Quasi-prepolymer L-55-0 — A quasi-prepolymer formed by reacting weights of Isonate 143L and THANOL SF-5505.
- Quasi-prepolymer P-55-0 — A quasi-prepolymer formed by reacting equal weights of PAPI 901 and THANOL SF-5505.
- 5 Quasi-prepolymer L-(5145-85)-0 — A quasi-prepolymer formed by reacting equal weights of Isonate 143L and experimental polyol 5145-85. 5
- THANOL SF-5505 — A 5500 molecular weight polyether triol containing approximately 80% primary hydroxyl groups.
- THANOL SF-6503 — A 6500 molecular weight polyether triol containing oxyethylene groups and approximately 90% primary hydroxyl groups. 10
- 10 L5430 Silicone Oil — A silicone glycol copolymer surfactant containing reactive hydroxyl groups. Product of Union Carbide. 10
- THANCAT DMDEE — Dimorpholinodiethylether.
- 15 Foamrez UL-29 — A stannic diester of a thiol acid. The exact composition is unknown. Product of Witco Chemical Co. 15
- Fluorocarbon 11-B — An inhibited trichlorofluoromethane.

Example I

- THANOL SF-5505 (12.0 pbw), ethylene glycol (6.44 pbw), L5430 silicone oil (0.2 pbw), THANCAT DMDEE (0.25 pbw), dibutyltin dilaurate (0.015 pbw) and Foamrez UL-29 (0.025 pbw) were 20
- premixed and charged into the B-component working tank of an Admiral 40 lb. (18 Kg) per min. low pressure mechanical mix foam machine. Isonate 143L (30.06 pbw) and P55-0 quasi prepolymer (5.24 pbw) were premixed and charged into the A-component working tank. The A-component temperature was adjusted to 80°F (27°C) and the B-component temperature was adjusted to 120°F (49°C). The machine was calibrated to deliver 4750 gms/min of B-component and 8870 gms/min of A-component 25
- (isocyanate to hydroxyl ratio=1.05). The ingredients were then mixed by a spiral type mixer turning at 4500 rpm and injected into a 15 in. by 15 in. by 0.150 in. (38 cm x 38 cm x 0.38 cm) steel mold preheated to 145°F (63°C) through a gating system which was built into the mold. A 3.2 second shot yielded a flat plaque having an overall density of about 62 pcf. (0.993 g. per cm³). Release time was 45 seconds from pour.
- 30 Two identical plaques were prepared and one was post cured at 250°F (121°C) for 1/2 hour while the other was post cured at 325°F (163°C) for 1/2 hour. After a week's rest at 75°F (24°C) and 50% relative humidity, 1 in. by 6 in. (2.5 x 15 cm) samples were cut from each of the above plaques. The samples were clamped at one end such that they projected horizontally with exactly 4.0 inches (10.1 cm) of sample remaining unsupported. After 1/2 hour the distance from the unsupported end to 35
- the base of the clamping fixture was measured. The fixture was then placed into a force draft oven at 325°F (163°C) for 30 minutes. After 30 minutes cooling, the distance from the end of the sample to the base of the clamping fixture was again measured. The difference in these two measurements (in inches) is termed the heat sag. The sample post cured at 325°F (163°C) exhibited a heat sag of 0.10 inches (0.25 cm) while the sample post cured at 250°F exhibited a heat sag of 0.42 inches (1.1 cm). 40
- The heat sag was also determined for identical plaques which were post cured at these temperatures for one hour. The heat sags were essentially identical to those obtained at 1/2 hour cure time. From these experiments it was concluded that the high temperature post cure caused a striking improvement in heat sag. The heat sag is analogous to past serviceability at the measured temperature. It is one of the standard tests for heat serviceability used by the automotive industry.

45 Example II 45

- The B-component of Example I was charged into the B-component working tank of a Cincinnati Milacron LRM-2 impingement mix RIM machine. Isonate 143L (29.0 pbw) and L55-0 quasi prepolymer (5.63 pbw) were premixed and charged into the A-component working tank. The A-component temperature was adjusted to 75°F (24°C) and the B-component temperature was adjusted 50
- to 100°F (38°C). The machine was then set to deliver the components at an injection rate of 3 lbs/sec (1.36 kg/sec) and at a weight ratio of 0.546 B-component/A-component. This represents an isocyanate index of 1.02. The components were then injected at an impingement pressure of approximately 900 psi (63.3 kg/cm²) into a steel plaque mold having cavity dimensions of 0.125 inches by 24 inches by 48 inches (0.3 x 60 x 120 cm). The mold temperature was set at 150°F (65.5°C). The parts were 55
- released in 60 seconds from pour. The plaques had a specific gravity of about 1.1.
- A number of identical plaques were prepared and cured within 15 minutes from pour for 1/2 hour at temperatures ranging from 250°F (121°C) to 350°F (177°C) in 10°F (5.5°C) increments. After one week's rest at 75°F (24°C) and 50% relative humidity, the heat sag of the samples cured at various temperatures were determined by the procedure outlined in Example I except an overhang of 6 inches 60
- (15.24 cm) instead of 4 inches (10.1 cm) was used in order to subject the samples to a more severe test so that smaller variations in heat sag could be seen. The data are presented graphically in Figure 1. As can be seen from the figure, the heat sag improved dramatically as the cure temperature is increased, with a leveling of the effect starting about 280°F (138°C). All plaques were characterized by

good dimensional stability upon removal from the cure oven (no significant distortion) until a cure temperature of 350°F (177°C) was reached at which point the plaques distorted badly.

Example III

The experiment in Example II was repeated except that a mixture of Isonate 143L (28.61 pbw) and P55-O quasi prepolymer (5.54 pbw) was substituted for the A-component of Example II. In this case, the B-component to A-component ratio was set at 0.554 (1.02 isocyanate index). The data are presented graphically in Figure 1. As can be seen from Figure 1, this RIM elastomer responded to cure temperature in a very similar manner to Example II. The significant difference is that the heat sag does not reach as low a value as Example II.

Example IV

The experiment in Example II was repeated except that a mixture of Isonate 191 (28.52 pbw) and P55-O quasi prepolymer (5.53 pbw) was substituted for the A-component ratio was set at 0.556 (1.05 isocyanate index). The data are presented graphically in Figure I. As can be seen from Figure I, this RIM elastomer responded to cure temperature in a very similar manner to Examples II and III. The significant difference is that the heat sag does not reach as low a value as in example II or III.

Example V

The experiment in Example II was repeated at 250, 300 and 340°F (121, 149 and 171°C) post cure temperatures, except that the chain-extender in the B-component was 1,4-butanediol (9.35 pbw). In this case, the B-component to A-component weight ratio was set at 0.631 (1.02 isocyanate index). The data are presented graphically in Figure I. As can be seen from Figure I, this RIM elastomer responded to cure temperature in a very similar manner to Examples II, III and IV. The significant difference is that the heat sag does not attain as low a value as in Examples II, III or IV. It should be noted, however, that the heat sag (cured at 325°F (163°C) measured at 250°F (121°C) on a 4 inch (10.1 cm) sample (industry standard) are excellent (0.03 in. (0.08 cm). Thus, this system is no doubt excellent for lower temperature applications.

Example VI

The experiment in Example II was repeated at 250, 279, 290, 310, 330 and 350°F (121, 132, 143, 154, 165.5 and 176°C) post cure temperatures except that a mixture of Papi 901 (27.58 pbw) and P55-O (5.35 pbw) was substituted for the A-component of Example II. In this case, the B-component to A-component ratio was set at 0.575 (1.05 isocyanate index). The data are presented graphically in Figure I. As can be seen from Figure 1, this RIM elastomer responded to cure temperature similarly to Example II, III, IV and V except that the improvement in heat sag obtained by high temperature cure is much less than in the other examples. It should also be noted that this elastomer is characterized by the poorest heat sag of all the elastomers tested.

More extensive testing was done on Examples II through VI. The following table is a summary of results.

Property	Example II		Example III		Example IV		Example V		Example VI	
Cure T, °F	250	330	250	330	250	320	250	350	250	310
°C	(121)	(165.5)	(121)	(165.5)	(121)	(160)	(121)	(177)	(121)	(154)
Isocyanate Index	1.02	1.02	1.02	1.02	1.05	1.05	1.02	1.02	1.05	1.05
Heat sag, in 6" (15.2 cm) overhand (in)	2.2	0.5	2.6	0.7	3.0	1.0	>4	2.0	3.3	2.4
(cm)	(5.6)	(1.3)	(6.6)	(1.8)	(7.6)	(2.5)	(>10.1)	(5.1)	(8.4)	(6.1)
Izod Impact, ft. lb/in. notch	6.5	7.6	7.3	7.4	5.3	4.6	6.3	4.6	3.2	2.8
Tensile, psi	5000	5070	4900	5100	5500	5700	4170	4450	5300	5500
(Kg. m ⁻²)(x 10 ⁸)	(3.52)	(3.56)	(3.44)	(3.59)	(3.87)	(4.01)	(2.93)	(3.13)	(3.73)	(3.87)
Elongation, %	123	127	133	138	106	97	128	93	63	67
Tear, pli	630	570	650	590	605	530	728	513	488	482
(g. cm ⁻¹)(x 10 ⁵)	(1.13)	(1.02)	(1.16)	(1.05)	(1.08)	(0.94)	(1.30)	(0.92)	(0.87)	(0.86)
Flexural modulus, psix 10 ³	147.0	146.7	136.5	129.8	157.3	151.3	124.6	124.2	158.4	158.9
(Kg. m ⁻²)(x 10 ⁶)	(103.3)	(103.1)	(95.97)	(91.26)	(110.6)	(106.4)	(87.6)	(87.3)	(111.4)	(111.7)
a) 75°F (24°C)	254.0	236.8	263.1	231.9	274.2	231.5	253.6	199.5	283.9	271.4
b) -20°F (-29°C)	(178.6)	(166.5)	(185.0)	(163.0)	(192.8)	(162.8)	(178.3)	(140.3)	(199.6)	(190.8)
c) 158°F (70°C)	82.0	93.8	75.1	86.1	87.5	92.2	59.9	76.5	87.0	91.7
d) 325°F (163°C)	(57.6)	(65.95)	(52.8)	(60.5)	(61.5)	(64.8)	(42.1)	(53.8)	(61.2)	(64.5)
Flexural modulus ratio	24.1	40.4	23.1	27.0	14.1	26.7	—	7.2	4.4	9.1
b/c	(16.9)	(28.4)	(16.2)	(19.0)	(9.9)	(18.7)	(—)	(5.1)	(3.1)	(6.4)
b/d	3.1	2.5	3.5	2.7	3.1	2.5	4.2	2.6	3.3	3.0
	10.5	5.9	11.4	8.6	19.5	8.7	—	27.7	64.5	29.8

Study of the above Table clearly shows that the isocyanate-chain extender reaction product and post cure temperatures have a dramatic effect on the properties of the resulting RIM elastomer. Generally, within each example, properties are better for the elastomers cured at higher temperature.

This is especially true of the thermal properties (heat sag, flexural moduli and flexural modulus ratios).

- 5 The elastomers cured at higher temperatures are more resilient (lower -20°F (-29°C) flexural modulus) at low temperature and stiffer at high temperature (high 158 and 325°F (70 and 163°C) flexural modulus). The elastomers cured at higher temperatures also show less temperature sensitivity in flexural modulus (lower flexural modulus ratios). It is clear from the Table that the absolute magnitude of the physical properties, especially the thermal properties, is partially controlled by the isocyanate chain-extender reaction product, properly post cured (post cured at higher temperature).
10 Examples II and III are preferred. The other examples show less improvement. From these considerations, it is evident that the isocyanate in the A-component should be relatively pure and either have or possess the capability of approaching a functionality of 2.0. Also, it is evident that the chain extender employed has a great effect on final heat properties. The RIM elastomer of Example V is less heat stable than the one of Example II. Prolonged post cured time or higher post cure temperature might make the RIM elastomer in Example V acceptable in heat properties. 15

- Figure II graphically presents the behavior of Izod Impact as a function of cure temperature and the composition of the isocyanate chain-extender reaction product. It is clear from Figure II that in some cases, the Izod Impact increases with increasing cure temperature (Example II) in some cases it decreases with increasing cure temperature (Examples IV and V) and in some cases remains rather constant (Examples III and VI). Also, the magnitude of the highest Izod Impact value attainable within an example seems to be a function of chain extender and isocyanate. Again, Examples II and III are preferred in this invention. From these considerations, it is again evident that the isocyanate in the A-component should be relatively pure and either have or possess the capability of approaching a functionality of 2.0. Also, the chain extender selected is critical to the final Izod Impact achieved. 25

- In Figure III, the flexural modulus at 325°F (163°C) is presented graphically as a function of cure temperature. These data correlate to the heat sag data in Figure I. The higher the flexural modulus at 325°F (163°C) the lower the heat sag measured at 325°F (163°C). Also, it is apparent that the chain extender and isocyanate chosen to form the isocyanate chain-extender reaction product is as important as the cure temperature. The same conclusions are drawn from this figure as far as selection of one temperature, chain extender and isocyanate are concerned as have been drawn from analysis of the data in Figures I and II. 30

- In Figure IV, the Flexural Modulus Ratio ($-20^{\circ}\text{F}/325^{\circ}\text{F}$ ($-29^{\circ}\text{C}/163^{\circ}\text{C}$)) as a function of cure temperature is presented graphically. These data show the importance of cure temperature and selection of isocyanate and chain-extender with respect to changes in Flexural Modulus. The lower the Flexural Modulus Ratio the less sensitive is the flexural modulus to changes in temperature. The same conclusions are drawn from this figure as drawn from Figures I—III. 35

Example VII

- The experiment of Example II was repeated except that the THANOL SF-5505 level was increased from 12 pbw to 16 pbw. This changed the flexural modulus at room temperature from about 140,000 psi ($9.87 \times 10^7 \text{ Kg/m}^2$) (Example II) to about 90,000 psi ($6.3 \times 10^7 \text{ Kg/m}^2$) (Example VII). The 6 inch (15.25 cm) heat sag at 325°F (163°C) for 1/2 hour was determined on samples cured at 250°F (121°C) (2.5 in. 6.35 cm) and 325°F (163°C) (0.6 in. 1.52 cm). Thus, the heat stability of the elastomer increased dramatically (lower heat sag) when cured at the higher temperature. This experiment extends the practice of our invention to lower flexural modulus RIM elastomers. 45

Example VIII

The experiment of Example II was repeated with the following formulation:

<i>B-Component</i>		<i>A-Component (1.02 Isocyanate Index)</i>		
THANOL SF-6503,	13.5 pbw	Isonate 143L,	26.32 pbw	
50 Ethylene Glycol,	6.44 pbw	P-55-0 (quasi-prepolymer)	5.21 pbw	50
Dibutyl tin dilaurate,	0.04 pbw			

- A sample cured at 325°F (163°C) for 1/2 hour exhibited a 4 inch (10 cm) heat sag (determined at 325°F (163°C) for 1/2 hour) of 0.15 inches (0.38 cm) while a sample cured at 250°F (121°C) for 1/2 hour had a heat sag (determined as above) of 0.93 inches (2.36 cm). The purpose of this experiment was to extend our invention to a different polyol (THANOL SF-6503) which has a higher molecular weight than THANOL SF-5505. 55

Example IX

The experiment of Example I was repeated with the following formulation:

<i>B-Component</i>		<i>A-Component (0.98 Isocyanate Index)</i>		
5	Experimental 4,000 molecular weight diol (4145-85),	12 pbw	Isonate 143L	28.9 pbw
	Ethylene glycol	6.44 pbw	L (5145-85)-0	
	L5430 Silicone oil	0.2 pbw	quasi prepolymer	5.6 pbw
	THANCAT DMDEE	0.25 pbw		
	Foamez UL29	0.025 pbw		
10	Dibutyl tin dilaurate	0.015 pbw		10

- A sample cured at 325°F (163°C) for 1/2 hour exhibited a 4 inch (10.1 cm) heat sag (determined at 325°F (163°C) for 1/2 hour) of 0.02 inches (0.05 cm) while a sample cured at 250°F (121°C) for 1/2 hour had a heat sag (determined as above) of 0.42 inches (1.1 cm). These results indicate the polyether polyols having a different internal structure are useful for this invention. The 5145-85 experimental diol is a 4,000 molecular weight diol based on mixtures of butylene oxide and ethylene oxide and capped with ethylene oxide to yield a primary hydroxyl content of about 90%.

Example X

The experiment of Example II was repeated with the following formulation:

<i>B-Component</i>		<i>A-Component (1.02 Isocyanate Index)</i>		
20	THANOL SF-6503	100 pbw	Isonate 143L	128.8 pbw
	Ethylene glycol	25.6 pbw		
	Dibutyl tin dilaurate	0.2 pbw		
	Fluorocarbon 11-B	2.0 pbw		

- Samples of the above elastomer cured at 325°F (163°C) for 1/2 hour exhibited a 6 inch (15.25 cm) heat sag (325°F (163°C) for 1/2 hour) of 1.3 inches (3.3 cm) while those cured at 250°F (121°C) for 1 hour had a heat sag (same conditions as above) of greater than 3.5 inches (8.9 cm). This example demonstrates the utility of this invention in improving the high temperature properties of RIM elastomers having an intermediate flexural modulus (about 60,000 psi (4.2 x 10⁷ Kg/m²)).

Example XI

The experiment of Example I was repeated with the following formulation:

<i>B-Component</i>		<i>A-Component (0.98 Isocyanate Index)</i>		
35	THANOL SF-5505	16 pbw	Isonate 143L	28.5 pbw
	Ethylene glycol	5.0 pbw	L-55-0 quasi prepolymer	5.52 pbw
	Monoethanolamine	1.44 pbw		
	L5430 Silicone Oil	0.2 pbw		
	THANCAT DMDEE	0.25 pbw		
	Foamez UL29	0.025 pbw		
	Dibutyl tin dilaurate	0.015 pbw		

- The above formulation reacted too rapidly to mold a complete plaque on this low pressure foam machine. A partial plaque was cut into two pieces. One piece was cured for 1/2 hour at 325°F (163°C) and the other piece was cured for 1/2 hour at 250°F (121°C). The 325°F (163°C) cured piece exhibited a heat sag (6 inch (15.25 cm) overhang heated for 30 minutes at 325°F (163°C) of 0.6 inches (1.5 cm) while the piece cured at 250°F (121°C) had a heat sag (same conditions as above) of 2.5 inches (6.3 cm). This experiment demonstrates the utility of still another chain-extender, monoethanolamine, in the practice of this invention. Monoethanolamine has one primary amine per molecule and is an example of a urea linkage forming chain extender.

Claims

1. A method of making a polyurethane elastomer of improved properties which comprises injecting an aromatic polyisocyanate, a polyol of above 500 equivalent weight and a chain-extending agent comprising a low molecular weight active hydrogen containing component having a functionality of at least two, into a mold cavity of a desired configuration, demolding the resulting molded article and post curing the demolded article at a temperature from 290 to 425°F (143 to 219°C).
2. A method as claimed in Claim 1, wherein post curing is carried out at a temperature of 310 to 350°F (154 to 177°C).

3. A method as claimed in Claim 1 or 2, wherein said chain-extending agent comprises ethylene glycol.
4. A method as claimed in any preceding claim, wherein said aromatic polyisocyanate is 4,4'-diphenylmethane diisocyanate.
- 5 5. A method as claimed in any preceding claim, wherein said polyol is a diol or triol having an equivalent weight of from 1000 to 3000 and contains at least about 50 percent of primary hydroxyl groups. 5
6. A method as claimed in any of Claims 1 to 4, wherein said polyol is a polyether polyol.
7. A reaction injection molded polyurethane article comprising the product obtained by a method 10 as claimed in any of the preceding claims. 10
8. A method as claimed in Claim 1 and substantially as hereinbefore described with reference to any of the Examples.
9. A polyurethane article as claimed in Claim 7 and substantially as hereinbefore described with reference to any of the Examples.

Printed for Her Majesty's Stationery Office by the Courier Press, Leamington Spa, 1980. Published by the Patent Office,
25 Southampton Buildings, London, WC2A 1AY, from which copies may be obtained.